ENVE 2061 BASIC FLUID MECHANICS Fluid Statics: Pressure At a Point Basic Equation for Pressure Field Change of Pressure in Static Liquid

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## **Lecture Notes from**

A Brief Introduction to Fluid Mechanics, 6<sup>th</sup> Edition, <u>Donald F.</u> Young, <u>Bruce R. Munson</u>, <u>Theodore H. Okiishi</u>, <u>Wade W. Huebsch</u>



## Learning Objectives:

 determine the pressure at various locations in a fluid at rest.

Question: how the pressure at a point varies with the orientation of the plane passing through the point?



Since we are considering the situation in which there are no shearing stresses, the only external forces acting on the wedge are due to the pressure and gravity.

Shearing stresses is zero; as the fluid mass moves as a rigid body; that is, there is no relative motion between adjacent elements.



Apply Newton's second law; F=m.a



Apply Newton's second law; F=m.a



#### Apply Newton's second law; F=m.a

$$\sum F_y = p_y \,\delta x \,\delta z - p_s \,\delta x \,\delta s \,\sin \,\theta = 
ho rac{\delta x \,\delta y \,\delta z}{2} a_y$$
  
 $\sum F_z = p_z \,\delta x \,\delta y - p_s \,\delta x \,\delta s \,\cos \,\theta - \gamma rac{\delta x \,\delta y \,\delta z}{2} = 
ho rac{\delta x \,\delta y \,\delta z}{2} a_z$ 

- Average pressures on the faces: ps, py, and pz
- Fluid Specific Weight: γ
- Density: ρ
- Accelerations: ay and az

**Note:** that a pressure must be multiplied by an appropriate area to obtain the force due to the pressure. It follows from the geometry that

 $\theta$ 

$$\delta y = \delta s \cos \theta$$
  $\delta z = \delta s \sin \theta$ 

Since we are really interested in what is happening at a point, we take the limit as  $\delta x$ ,  $\delta y$ , and  $\delta z$  approach zero (while maintaining the angle  $\theta$ ), and it follows that

$$p_y - p_s = 
ho a_y \, rac{\delta y}{2} 
onumber \ p_z - p_s = (
ho a_z + \gamma) \, rac{\delta z}{2}$$

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ho a_z+\gamma)\,rac{\delta z}{2}$$

Since we are really interested in what is happening at a point, we take the limit as  $\delta x$ ,  $\delta y$ , and  $\delta z$  approach zero (while maintaining the angle  $\theta$ ), and it follows that

$$p_y = p_s$$
  $p_z = p_s$ 

ps = py = pz

# Conclusion: pressure at a point in a fluid at rest, or in motion, is independent of direction as long as there are no shearing stresses present. Pascal's law

Pascal's law, named in honor of Blaise Pascal (1623–1662), a French mathematician who made important contributions in the field of hydrostatics.

2<sup>nd</sup> Question: how does the pressure in a fluid in which there are no shearing stresses vary from point to point?

consider a small rectangular element of fluid removed from some arbitrary position within the mass of fluid of interest

There are two types of forces acting on this element: **surface forces due to the pressure** and a **body force equal to the weight of the element**.

Other possible types of body forces, such as those due to magnetic fields, will not be considered.



2<sup>nd</sup> Question: how does the pressure in a fluid in which there are no shearing stresses vary from point to point? The resultant surface forces in the x and



direction are

$$\delta F_x = -rac{\partial p}{\partial x} \; \delta x \; \delta y \; \delta z \; \; \delta F_z = -rac{\partial p}{\partial z} \; \delta x \; \delta y \; \delta z$$

The resultant surface force acting on the element due to pressure can be expressed in vector form as

$$\delta \mathbf{F}_s = \delta F_x \hat{\mathbf{i}} + \delta F_y \hat{\mathbf{j}} + \delta F_z \hat{\mathbf{k}}$$

$$\delta \mathbf{F}_s = -igg( rac{\partial p}{\partial x} \hat{\mathbf{i}} + rac{\partial p}{\partial y} \hat{\mathbf{j}} + rac{\partial p}{\partial z} \widehat{\mathbf{k}} igg) \, \delta x \; \delta y \; \delta z$$

 $\hat{\mathbf{i}}, \hat{\mathbf{j}}$ , and  $\hat{\mathbf{k}}$  are the unit vectors along the coordinate axes

$$rac{\partial p}{\partial x} \hat{\mathbf{i}} + rac{\partial p}{\partial y} \hat{\mathbf{j}} + rac{\partial p}{\partial z} \widehat{\mathbf{k}} = 
abla p$$

$$abla \left( \; 
ight) = rac{\partial \left( \; 
ight)}{\partial x} \hat{f i} + rac{\partial \left( \; 
ight)}{\partial y} \hat{f j} + rac{\partial \left( \; 
ight)}{\partial z} \widehat{f k}$$

Surface and body forces acting on small fluid element.

The resultant surface force in the y direction is  $\delta F_y = \left(p - rac{\partial p}{\partial u}rac{\delta y}{2}
ight)\delta x\delta z - \left(p + rac{\partial p}{\partial u}rac{\delta y}{2}
ight)\delta x\ \delta z$ 

$$\delta F_y = -rac{\partial p}{\partial y} \delta x \; \delta y \; \delta z$$

$$\delta \mathbf{F}_s = \delta F_x \hat{\mathbf{i}} + \delta F_y \hat{\mathbf{j}} + \delta F_z \hat{\mathbf{k}}$$

$$\delta F_x = -rac{\partial p}{\partial x} \ \delta x \ \delta y \ \delta z \ \ \delta F_z = -rac{\partial p}{\partial z} \ \delta x \ \delta y \ \delta z$$

 $\delta F_y = - rac{\partial p}{\partial y} \delta x \; \delta y \; \delta z$ 

$$\delta \mathbf{F}_s = -\left(rac{\partial p}{\partial x}\hat{\mathbf{i}} + rac{\partial p}{\partial y}\hat{\mathbf{j}} + rac{\partial p}{\partial z}\hat{\mathbf{k}}
ight)\delta x\ \delta y\ \delta z$$

$$rac{\delta {f F}_s}{\delta x \ \delta y \ \delta z} = - 
abla p$$

The resultant surface force acting on a small fluid element depends only on the pressure gradient if there are no shearing stresses present.

Since the z axis is vertical, the weight of the element is

$$-\delta \mathscr{W} \widehat{f k} = -\gamma \ \delta x \ \delta y \ \delta z \ {f k}$$

the negative sign indicates that the force due to the weight is downward (in the negative z direction).

Newton's second law, applied to the fluid element

$$\sum \delta \mathbf{F} = \delta m \mathbf{a}$$

**Σ** δF represents the resultant force acting on the element, a is the acceleration of the element, and δm is the element mass, which can be written as  $\rho$  δx δy δz. It follows that

$$\sum \delta \mathbf{F} = \delta \mathbf{F}_{\circ} - \delta \mathscr{W} \widehat{\mathbf{k}} = \delta m \mathbf{a}$$

$$-
abla p - \gamma \widehat{f k} = 
ho {f a}$$

general equation of motion for a fluid in which there are no shearing stresses

$$rac{\partial p}{\partial x}=0 \qquad rac{\partial p}{\partial y}=0 \qquad rac{\partial p}{\partial z}=-\gamma$$

For a fluid at rest, 
$$\mathbf{a} = 0$$
,  $\nabla p + \gamma \hat{\mathbf{k}} = 0$ ,  $\nabla p = -\gamma \hat{\mathbf{k}}$ 

$$\frac{\partial p}{\partial x}\,\mathbf{\hat{i}} + \frac{\partial p}{\partial y}\,\mathbf{\hat{j}} + \frac{\partial p}{\partial z}\,\mathbf{\hat{k}} = \nabla p = -\gamma\mathbf{\hat{k}}$$

 $\frac{\partial p}{\partial x} = 0 \qquad \frac{\partial p}{\partial y} = 0 \qquad \text{we move from point to point in a horizontal plane (any plane parallel to the x-y plane), the pressure does not change.}$ 

Z,

$$rac{\partial p}{\partial z} = -\gamma \qquad \longrightarrow \qquad rac{dp}{dz} = -\gamma$$

can be written as the ordinary differential equation, since p depends only on z,

For liquids or gases at rest, the pressure gradient in the vertical direction at any point in a fluid depends only on the specific weight of the fluid at that point.

$$\frac{dp}{dz} = \frac{\Delta p}{\Delta z} = -\gamma$$

## **CHANGE OF PRESSURE: INCOMPRESSIBLE FLUIDS**



most engineering applications the variation in g is negligible

In general, a fluid with constant density is called an incompressible fluid.

$$\int_{p_1}^{p_2}dp=-\gamma\int_{z_1}^{z_2}dz$$

$$p_2 - p_1 = -\gamma(z_2 - z_1)$$

h is the distance,  $z_2 - z_1$ , which is the depth of fluid measured downward from the location of  $P_2$ 

h is called the pressure head and is interpreted as the height of a column of fluid of specific weight  $\gamma$  required to give a pressure difference p1 – p2.

$$p_1-p_2=\gamma(z_2-z_1)$$
  
h h  
to  $p_1-p_2=\gamma h$ 

the pressure difference between two points can be specified by the distance h,

## **CHANGE OF PRESSURE: INCOMPRESSIBLE FLUIDS**



h is called the pressure head and is interpreted as the height of a column of fluid of specific weight  $\gamma$  required to give a pressure difference p1 – p2.

Pressure difference = 69 kPa It can be expressed in terms of **pressure head as 7 m** of water 69 kPa = 9.81 kN/m<sup>3</sup>x 7 m or 69 kPa=133kN/m<sup>3</sup>x 0.518 m (or 518 mm)

 $\gamma_{Hg}$ = 133 kN/ m<sup>3</sup>,  $\gamma_{water}$ = 9.81 kN/ m<sup>3</sup>

a 7 m-tall column of water with a cross-sectional area of 6.5 cm<sup>2</sup> weighs 4.5 kg.

#### **CHANGE OF PRESSURE IN STATIC FLUIDS : INCOMPRESSIBLE FLUIDS**



most engineering applications the variation in g is negligible

In general, a fluid with constant density is called an **incompressible fluid**.

$$\int_{p_1}^{p_2} dp = -\gamma \int_{z_1}^{z_2} dz$$

$$p_2-p_1=-\gamma(z_2-z_1)$$





## **CHANGE OF PRESSURE: COMPRESSIBLE FLUIDS**

Gases such as air, oxygen, and nitrogen as being **compressible fluids** because the density of the gas can change significantly with modest changes in pressure and temperature.

> it is necessary to consider the possible variation in  $\gamma$  before the equation can be integrated

compared to liquids variation of pressure with Ideal Gas Law elevation change is negligible.

$$\frac{dp}{dz} = -\frac{gp}{BT}$$

 $p = \rho RT$ 

$$\int_{p_1}^{p_2} rac{dp}{p} = \ln \; rac{p_2}{p_1} = -rac{g}{R} \; \int_{z_1}^{z_2} rac{dz}{T} \qquad iggarage$$

g and R are assumed to be constant over the elevation change from  $z_1$  to  $z_2$ .

$$p_2=p_1\exp\left[-rac{g(z_2-z_1)}{RT_0}
ight]$$

**Note:** Specific weight of the gases so small

Assumption: the temperature has a constant value  $T_0$  over the range  $z_1$ to  $z_2$  (isothermal conditions),

## **CHANGE OF PRESSURE: COMPRESSIBLE FLUIDS**

In 2010, the world's tallest building, the Burj Khalifa skyscraper was completed and opened in the United Arab Emirates. The final height of the building, which had remained a secret until completion, is 828 m.

Find: a) Estimate the ratio of the pressure at the 828 m top of the building to the pressure at its base, assuming the air to be at a common temperature of 290°K. b) Compare the pressure calculated in part (a) with that obtained by assuming the air to be incompressible with  $\gamma$ =11.99 N/m3 at 1 atm (abs) (values for air at standard sea level conditions).



Note that there is little difference between the two results. Since the pressure difference between the bottom and top of the building is small, it follows that the variation in fluid density is small and, therefore, the compressible fluid and incompressible fluid analyses yield essentially the same result.